

# International Institute For Cotton Technical Research Division

Manchester

**Research Record No. 81** 

# The Effect Of Varying Knitted Loop Length And Take-Down Tension On The Ease Of Processing Of Knitted Fabrics

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Key Words: Knitgoods, Knitting Variables, Knitgoods Finishing, Take-Down Tension.

**Digital Version:** 

March 2009 spreadsheet is *tdtens.xls* 

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#### Note:

Figure 3 is new for the Digital Version. The corresponding spread-sheet is *tdtens.xls* 

## Introduction

The effect of knitting machine take-down tension on the potential relaxation characteristics of knitted structures has been investigated in some detail by Black (1).

Although fabrics produced on a knitting machine from a standard yarn and at a constant knitted loop length have a fixed fully relaxed structure, the actual knitted structure can vary considerably due to the inconsistency in the operation of the take-down mechanism.

The purpose of this exercise was to examine whether these inconsistencies cause undue problems to the finisher, whose main consideration is one of trying to eliminate these distortions created by the knitting machine.

This was somewhat of a quick and crude investigation, aimed at giving an indication as to whether a problem does exist and whether a more detailed investigation is required.

The information was also required to clarify several points being made in a forthcoming paper on knitgoods finishing.

## **Outline Of Investigation**

The aim was to monitor what actually happens to the knitted structure when it is subjected to the rigours of a winch treatment of up to 12 hours duration.

As the winch subjects the fabric to some degree of length tension, only the change in lengthways dimensions was considered in this investigation. To facilitate ease of measurement, fabrics were made with reference threads built into them. This was achieved by using coloured yarns on particular feeders: by measuring the change in distance between (a number of) the stripes, a fairly accurate indication as to changes in length dimension could be obtained.

This method of approach, rather than the measurement of course spacings had to be adopted since the measurements were being taken in the winch with the fabric at a temperature of around  $90^{\circ}$ C.

## **Fabric Variables**

For this exercise, a 24 gauge single jersey fabric produced on the Monarch XL-JS machine was used.

Four lengths of fabric were made which covered two tightness factors, each knitted with high and low take-down tensions. Each variable was readily identifiable by means of an individual stripe and colour pattern.

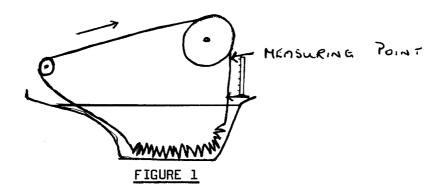
The knitting specifications for the various fabrics are given in *Table 1* in the Appendix.

## Procedure

The four lengths of fabric were sewn together to form a single rope which was loaded into the Leemetal winch. The winch contained water, with the addition of 2g/l Synperonic NX (detergent), sufficient to give a liquor to goods ratio of 20: 1.

The speed of the fabric in the winch was set at 60 ypm. The temperature of the water was raised from cold to  $90^{\circ}$ C and maintained at this temperature throughout the investigation.

The changes in fabric dimensions were observed by stopping the machine at regular intervals and measuring the distance between five coloured stripes. An average of three measurements taken at different places throughout the individual pieces was used. The point at which the measurement was taken is indicated in *Figure 1*. This point was chosen because of ease of access and also because of the minimum of fabric handling which could cause some distortion to the structure.



Measurements were taken at 15 minute intervals for the first hour and then every subsequent hour until the sixth hour. For the remaining six hours the measurements were taken every other hour.

The reason for a 12 hour cycle was that this kind of treatment is not uncommon particularly when fabrics have to be stripped and redyed.

After the 12 hours, the winch was stopped, the liquor dropped and fresh cold water added. The fabric was removed from the winch after a short rinse, hydro-extracted and carefully slit by hand. Drying was carried out on the Artos stenter, the width settings used corresponding to the fully relaxed widths which had previously been determined by washing and tumble drying.

The overfeed was set at an arbitrary level and was not adjusted during the passage of the fabric.

Samples of the grey-state fabrics and also after stenter drying were submitted to the laboratory for testing. Results are given in *Table 3* and *Table 4*. *Table 2* gives the details of the measurements taken during the winch cycle. These are shown graphically in *Figure 2* and *Figure 3*.

#### **Discussion Of Results**

From the graphs, the following points are shown quite clearly.

- 1. Where a low take-down tension has been used, the fabric extends to a considerable degree, even after a short period in the winch. Where high take-down tension has been used, this additional extension is much less.
- 2. Any extension in the winch occurs within the first hour of treatment. Leaving the fabric in the winch for extended processing periods does not cause any additional extension.
- 3. The differences in grey-state structure brought about by variable take-down tensions are

easily eliminated once the fabric is wet treated in the winch.

4. Once the fabric is removed from the winch and hydroextracted, there is a considerable relaxation in the distortions which have occurred.

From this short study, the effect of varying take-down tension on the knitting machine does not pose any additional problems to the finisher.

Because fabrics of different tightness factors have been used in this trial, we have had the additional opportunity of observing how the knitted loop length affects the ease of processing.

*Table 3* gives the comparative test data of the machine state fabrics: the differences in relaxation characteristics for the two tightness factors are very clear to see. What is also apparent is the effect the tightness factor has on spirality angle, particularly after relaxation.

*Table 2* gives the measurements taken during the scouring operation. If the equilibrium measurements from the winch are compared with the relaxed-and-tumble-dried measurements, the degree of extension from the fully relaxed state is found to be as follows.

	Distance betwee	en 5 stripes, cm	
Tightness Factor	Fully Relaxed	In the Winch	Extension, %
16.42	15.3	17.7	15.7
13.41	19.6	25.7	31.1

The fabric with the higher tightness factor is therefore likely to be easier to finish than the fabric with the lower tightness factor.

*Table 4* gives the test results obtained on the stenter dried fabrics and the difference is clear to see in the residual length shrinkage figures.

#### Conclusion

This has been a rather quick and crude evaluation, to attempt to obtain some quick answers. It has however produced some interesting results and a more detailed study ought to be undertaken. This should include a study of the effect on chemical treatments such as bleaching on the fully relaxed structure.

#### References

1. DH Black: AATCC Symposium Report - "*Knit Shrinkage, Cause, Effect and Control*", p69 (October 1973).

Machine:	Monarch XL-JS Single Jersey 24g, 26" Diameter, 60 feeds, 1920 Needles 1/24 Ne HSP, 24.6 tex:							
Yarn:								
Marker threads:	1/24 Ne	- Brown						
Piece No	1	2	3	4				
Tightness Factor, K	16.42	16.42	13.41	13.41				
Stitch Length, cm	0.301	0.3021	0.3698	0.3698				
Yarn Tension, g	3-5	3-5	3-5	3-5				
Stretcher Board	constant	constant	constant	constant				
Take-down Tension	Min: <sup>1</sup> /2 weight	Max: 3 <sup>1</sup> /2 weights	Min: 1/2 weight	Max: 3 <sup>1</sup> /2 weights				
Marker thread	1 feed Orange	2 feeds Orange	1 feed Brown	2 feeds Brown				
On-machine CPI	48	41	29	27				
On-machine WPI	27	29	27	28.5				
Dist. between stripes, cm	3.2	3.8	5.2	5.8				
Width at TD roller, cm*	~85	~81	83	80.5				
Width on roll*	~85	~82	83	82				

# Table 1: Knitted Fabric Specifications

\* Width measurements on pieces 1 & 2 are approximate due to creasing.

 Table 2: Measurements Taken

MEASU RING		TIGHTINESS FACT	ror 16.42	TIGHTNESS FACTOR 13.41				
Poir	NT	LOW TENSION	HIGH TENSION	LOW TENSION	HIGH TENSIO			
AFTER DRY	KMITTING RELAXE)	14.5	16.4	23.7	ଥି <u></u> ତ -			
JINGI	15 MINS	16.7	17.4	23.0				
	30 MINS	17.7	18.1	25 8	26.7			
	45 mins	17.7	17.9	25.6	26.3			
	60 Mins	17.7	17.9	25.4	25.5			
	2 Howks	17.4	17.8	<i>ఎ</i> క క	as <u>s</u>			
100-1433 ( 1 - 100-149)	3 Howes	17.4	17.8	ସ୍ଠ- 3	25.6			
	4 Houres	17.5	17.8	25.4	25.8			
	5 Homes	176	17.6	25.5	25.9			
<b>Language of Sector</b>	6 Hones	176	17.7	25.5	25.7			
• <u></u>	8 Hones	17.8	17.7	a <i>s s</i>	86.1			
	10 1+0~es	17.8	17.8	ଚଽ୶	26.1			
	12 Howles	. 17.7	17.7	25.6	<u> </u>			
	OEXTRACTINE	. 17.0	17.0	Q3·2	JJ.J			
	RELAXED.							
AFTER	RENAXING 1BAE DETING	. 15.3	15.4	19.6	19.6.			

NOTE Figures given relate to the distance - considering fire single feeder shipes of 5x 60 words = 300 words.

# Table 3: Grey-State Test Data

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DATE: 1

TESTS REQUIR	RED	1	TIGHT	NESS FF		16.42	- Ét	SAMF	LETIGHT	NESS FACT	or 1	3.41
ن <u>محمد والمناسم من من من من من من من معمد من محمد مع</u>		V	TENSIDA	95%CL	TENSION	95%CL		95%CL	MINIMUM	95%CL	TENSION	
SHRINKAGE I	length	1	4.4%+		4.97%				14.86%		19.46%	
	⊿idth	$\top$	26.0%		23.1%				11.29%.		10.85%	
ABRIC WEIGHT	BW		166.7	5.15	156.2	7.62			134.7	6.38	119	4.30
	ΑW		210	4.64	203.4	5.09			174.6	5.73	175.2	5.85
:/3_#4	BW		54.6	0.35	49.8	0.70			35.7	0.43	33.7	0.44
	AIJ	Τ	51.9	0.46	52.1	0.22			40.5	0.36	40.8	0.55
1/3_041	BW		27.2	0.31	27.1	0.31			27.6	0.25	27.2	0.41
	AW		36.4	0.31	36.2	0.30			31.6	0.31	31.7	0.33
STITCH LENGTH	ອຟ		2.94	0.009	2.93	D.011		-	3.59	0.021	3.59	0.05
~~ .	AW		2.93	0.016.	2.89	0.031			3.60	0.023	3.51	0.03
BURST STRENGTH	B₩										<u> </u>	
	AW	]										ļ
PIRALITY ANGL	S BW		13.18	کھ٠٥	13.50	1.41			13.7	1.24	15.2	0.87
	AW		14.15	1.06	14.85	1.08		İ	23.02	1.22	22.8	1.15
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COMMENTS:								FABRIC	DETAILS:			

GREY STATE TEST RESULTS

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#### Table 4: Finished Fabric Test Data

TESTS REQUIRED		TIGHTNESS			16.42	•		PLE TIGHTINESS FA		TETOR	13.4
	$\bigvee$	MINIMUM TENSION	95%CL	TENSION	95%CI.		95%CL	MINIHUH TENSION	95%CL	TENSION	95%0
SHRINKAGE length		13.75		15.97				21.5		23.13	
width		1.8		2.45				1.06		1.19	
ABRIC WEIGHT BW											
AW		198		198				169.4		166.6	
13-ett inch BW		43.5		42				31.9		29.3	
Au	<u> </u>	50.2		49.8				39.5		39.6	
1/3-TT INCH BW		36.3		36.1				31.7		32.3	 
AW		37		36.6				31.1		30.9	
GTITCH LENGTH BW										L	
<u> </u>		2.83		2.91				3.54		3.51	L
BURST STRENGTH BW	ļ			-					a Thurbul a singly in a sustained in		l
AW	ļ										
PIRALITY ANGLES BW	<u> </u>									ļ	
AW	L										
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LE TARN LOUNT AN	<u> </u>	24.7		24.3			<b></b>	23.9		23.9	
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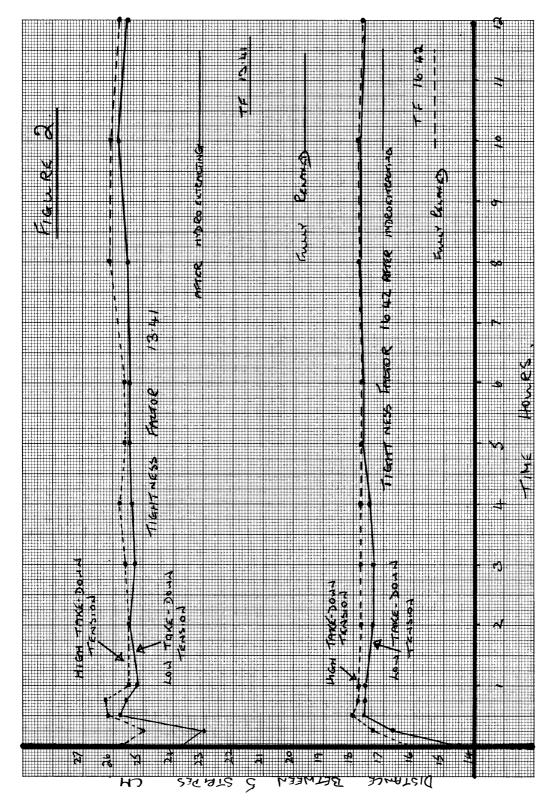


Figure 2: Graphical Representation of Measurements



