

Research Record No 175

The Finishing Of 28 Gauge Interlock

A description of the processing carried out at Meridian during 7th - 11th February 1983

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1. Introduction

Research Record No. 162 describes the production of two complete 15-quality blocks of 28g interlock fabric at the Courtaulds Research Group at Spondon. The knitting was directly supervised by TRD personnel and individual pieces of length approximately 50 metres were produced.

The reasons for wishing to carry out a 28g series are described in Research Record No. 182, but briefly, the main reason was to establish conclusively whether or not there is an independent gauge effect. With the single jersey exercise three gauges were examined whereas with the double jersey project only 20g interlock was initially examined.

2. Trial Outline

Since carrying out the Central Project processing in 1978 there have been a number of changes in the way in which Meridian process their fabrics. In particular, wet stretching of fabrics on the Calator Airtex is now almost routine. To adopt their current processing route would introduce another variable into the scheme and therefore since the main aim was to examine gauge effect it was decided to process these two sets of 28g interlock fabrics in as near an identical manner to the 20g interlock fabrics as possible. In addition, it was felt that more information was required on winch processing since in the original CP78 project winch processing was only considered as a minor route.

Since two complete sets of fabric were available for processing it was decided that one set should be winch dyed and the other set winch bleached.

3. Fabric Coding

Each individual fabric variant was coded using the system established at the start of the central project processing, i.e. a combination of yarn count and stitch length: e.g. 60/248

yarn count 1/60's Ne

stitch length 0.248 cms

4. Calculation of Finishing Targets

In Research Record No. 162, a series of equations is given to describe the behaviour of grey interlock fabrics, in the range 20-28 gauge, during a relaxation treatment, and to provide predictions for the relaxed structures of these fabrics in the grey state.

From previous experience, it could be expected that these equations would not, by themselves, provide a sufficiently accurate basis for the calculation of finishing targets (widths and course spacings) for winch processed goods. It was thought, however, that these equations might be used if suitable correction factors could be derived.

In Research Record No. 121, Tables 23, 24, 27 and 28, results are given for the relaxed courses and wales of a series of 20g interlock fabrics in the grey, winch-bleached and winch-dyed states. Although only six fabric structures were included in this study, it was considered that these results should give some insight into the relative behaviours of grey and winch processed interlock, and

a study of these data produced the following approximate relationships.

- 1. Courses/3cm (winch-processed, relaxed) = 0.91 x courses/3cm (grey, relaxed)
- 2. Wales/3cm (winch-processed, relaxed) = wales/3cm (grey, relaxed)

The equations given in Table 8, Research Record No. 162, for 20 and 28g fabrics, were then used to calculate, for the 28g fabrics.

- 1. grey, relaxed course and wale spacings;
- 2. winch processed, relaxed course and wale spacings, using equations 1 and 2 above
- 3. targets for finishing, assuming residual shrinkages of 10% in both length and width.

The results of these calculations are given in the table below.

		GREY RELAXED		FINISHED F	RELAXED	TARGETS		
		Courses/3cm	Wales 3 cm	Courses/3cm	Wales 3 cm	Courses/3cm	Width cm tub	
1.	70/236	70.2	62.1	63.9	62.1	57.6	70.6	
2.	70/248	66.3	61.1	60.3	61.1	54.5	71.9	
3.	70/260	62.8	60.0	57.1	60.0	51.6	73.1	
4.	60/236	71.1	59.7	64.7	59.7	58.3	73.5	
5.	70/273	59.3	59.0	54.0	59.0	48.8	74.4	
6.	60/248	67.2	58.6	61.2	58.6	55.2	74.9	
7.	70/287	56.0	58.2	51.0	58.2	46.1	75.6	
8.	60/260	63.7	57.6	58.0	57.6	52.3	76.2	
9.	60/273	60.2	56.6	54.8	56.6	49.4	77.6	
10.	50/236	72.2	56.6	65.7	56.6	59.2	77.6	
11.	60/287	56.9	55.6	51.8	55.6	46.7	79.2	
12.	50/248	68.3	55.4	62.2	55.4	56.2	79.0	
13.	50/260	64.8	54.4	59.0	54.4	53.2	80.7	
14.	50/273	61.4	53.4	55.9	53.4	50.4	82.2	
15.	50/287	58.0	52.4	52.8	52.4	47.6	83.7	

During the actual processing, difficulties were experienced which are described later in the report.

New target width figures were therefore assigned which were calculated from the measured grey relaxed wales/3cm by building in a 15% width shrinkage figure.

5. Description of Processing

Prior to processing in the winches, the individual rolls of fabric were plaited off and marked at both ends with their identifier. To augment the dye lots, half-pieces of standard 20g interlock were added to each winch load. As well as contributing to total fabric weight they would also be replicates for the original CP78 processing of this particular fabric variant.

Dyelot 1 was designated for dyeing to a blue shade using 2% Procion Blue HE GN. To obtain the brightness of shade it is usual at Meridian to pre-bleach the fabric as part of the preparation sequence in the winch. Following dyeing, the fabric is softened in the winch using cationic softener/lubricants.

Lot 2 was subjected to the full Meridian treatment for obtaining a good optic white. This consisted of a combined hypochlorite/peroxide bleach in which an optical brightening agent was included. Following rinsing, a cationic softener was again applied in the winch.

Details of the dyeing of the blue shade are given in Table 1 and details of the bleached lot are given in Table 2.

After removal from the winches the fabrics were dewatered in the centrifuge and sorted into order of ascending width ready for dyeing. Drying was carried out on the Pegg drying/finishing machines with target widths 2cm below the finished target width to allow sufficient scope for the calender.

It became obvious that the fabric wanted to be considerably wider than the target widths. In order to attain the required widths from the dryer, the level of overfeed applied had to be kept to a minimum to prevent jamming and creasing on the stretcher frame. As a consequence the number of courses that it was possible to attain was well below what should be possible from the dryer.

To ensure consistency, both winch lots were dried to the same targets even though it was clearly obvious that the width targets were too low.

Prior to calendering, the width targets were reviewed but this meant that a considerable number of the variants would now be too wide for the Tubetex compactor. The decision was therefore taken to omit compaction from the sequence and to attempt to calender the fabrics to the new finished targets which in most cases meant an increase in width of around 4-5cms.

Even though the fabrics were calendered without any trouble it was clear that the fabrics needed to be finished even wider.

In fact, when the fabrics were sampled some two hours later, many of the fabrics had increased their width by up to $1\frac{1}{2}$ cm.

Measurements of courses/3cm and width were taken for all fabric variants at every stage of processing. These are given in Table 3 (Winch-dyed) and Table 4 (Winch-bleached).

6. Conclusions

The major problem experienced during the processing of these two winch-lots was one of width

control. At all stages the fabrics seemed to want to be wider than their calculated target widths. Consequently, great difficulty was experienced in obtaining sufficient courses in the fabric to ensure low length shrinkage figures. Even when the targets were increased the fabric showed a tendency to grow in width between calendering and sampling by up to $1\frac{1}{2}$ cm.

It would therefore seem reasonable to expect the fabrics to have low residual width shrinkage figures at the testing stage.

Table 5 shows the actual shrinkage figures and in fact relatively high width shrinkage figures have been obtained (11-18%) which is rather surprising and to some extent disconcerting.

Further investigation into this problem is necessary.

THE LAST TELES INTAL T DYELOT 000001 1 HETRIC TALLE WINCH - 4 -The second stands on the I OFDEE 25 3414 0311 8110 149 NTHE MARE DO NOT MAKE WALLTY CORFERENCE A HINE COMMENTS MACHINE S Prochame JBPSHELA tarent fime 10 MN PPL BLEACH ----ADD ADD 🤟 GRM 100015 5.00 CAUSTIC SOLA LIO. 8050 - 6440 1 ----HYDROGEN PEROXIDE STORE 1 1 1 THE BOLL TAKING 30 MINUTES, BOIL FOR 30 MINUTES AND SHOW. ALIZE WITH GRM ADD ADD 1 JO 42 2.00 3 HYDROS & ACENCACIP ANC 4 OR 20 MINUTES AT 'O' , WASH OFF WELL. BATH DYL FION PROCION DYES 1/3 80 GPL SALT T AT 50 C - And the second second second ORM AUD ADD J10108 2.0000 - FROCION BLUE BECH 3220.000 1. 1 ER 10 MINS, RUN FOR CO MINS GRM ADD ADD 193200 / 1 99.00 SALT BAGGED TABLE 1 AVER 20 MINS, MUN 10 MM 1 12 -

Willing and ------. . DE REMAININ MER 20 STAS RUN 10 KER SOMIN ADD 🐸 ADD 1444 1 AMERICO E 2.6.2 0900 019 APH 1 IN SOUR ASH IN THU PART OVER TO HINS H TON BACK OUP ADD ADD ORM 5000082 50 10 1 HIREY R 1207 1 TRE TO THE BOIL - BOIL FOR 20 MINUTES. TTON SOFTEN -ANDOLURE GRT COLD ADD SANDACLD RAISE TO 40'C SANDOLUBE KUN "O MINS AND HOW ADD ADD GRM -----....... ----3220 1 1 SANDACID 8218E .00 % 040102 SANDOLUBE LSC 1 3220 1 ·C 10103 2.00 7 . . TABLE 1 (LONT.)

MACHINE WIE 1 1 CUSTOMER 1.1.C. I DYELOT IICOO.' I WEIGHT 157+ I SHADECODE OFTIC 401 ORDER TRIAL 1 VOLUME 3140 QUALITY COCC+ SHADENAME OPTIC STANDARD ----QUALITY COMMENTS Y i. MACHINE COMMENTS MACHINE : Weins Procedure COOPTICW Tardet Time 5 TIYE BATH - BLEACH/DYE -BLEACH/OPTIC WHITE START COLD GRM ADD ADD 1570 + 7000019 1.00 % CONTAVAN HW the state of the second states with ADD, RUN 10 MINS ADD ORM ADD -----13000092 12.00 % SODTUM HYPOCHLOPITE 15910 1 DD.RUN 20 MINS GRM ADD ADD 7850 1 21000015 5.00 % CAUSTIC SODA LIQ. ADD 1/2. RUN 15 MINS -RAISE TO 60'C OVER 15 MINS, RUN 15 MINS IDD REST OF CAUSTIC AND GRM ADE ATO 2420 1 23000041 5.90 % HYDROGLA FEROXIDE STORE ----ADD, RUN 10 MINS ORM ADD ADD TABLE 2. 1095 000 1 1 25060106 0.2000 : PHOTINE 121

VISE TO BOIL OVER 30 MINS VIL FOR 60 MINS AND SHOW	
TIC HYDROS	
SH OFF WELL, COLD AND HOT	
	GRM ADD ADD
000042 1.50 % HYDROS R	.355.1 1
D, RUN 20 MINS AT 60°C Sh off Well Again	
TTON SOFTEN ALCOLUBE NO EULYSIN	
D	
	SRM ADD ADD
000007 1.50 % ALCOLUBE BSL :00	2355 1 1
Light to East	
Hilling and the second se	

	TA	RGET	5	PEGG	R	CALKA	DER	SAHIR	NE.
VARIANT	GI	WID	TH	1/3		43	WIJTH	·/3	NIJTH
	73	DRIGINAL	REVISED		חופוש				
38/338		61	61	342	592	37	61	37	61
70/236	575	70'2	フジュ	522	682	53£	752	55	77
70/248	54%	72	762	46%	70	49	762	49=/50	78%
170/260	512	73	フフネ	442	7/2	452	772	472	79
160/236	582	732	78	53	712	55	78	562	79
170/273	49	742	79	40	72:	43	79	44	812
10/2/8	55	75	80	472	73	51	80	51	80
70/287	46	75%	802	362	732	42 2	802	40	81
10/201	52'2	76	802	445	74	50	80%	472	81
1	1.91	77	81	40	75%	44	812	45	85
50/236	59	772	82	54%	75%	56%	82	562	832
160/287	465	79	82	392	772	42 1	82	41	85
1/100	10	79	82:	51	77	53 2	832	54%	84
20/248	56	80%	85	48	782	. 50	85	50	87
50/260	55	47	86	43%	80		86	46	88
50/273	50%	- 02			0.6	1.1	87	44	89
50/287	47:	2 835	87	415	812	45	07		

WINCH DYED

TABLE 3

- A Participal	TA	RGETS	5	PEGG	e	CULKN	DER	SAMP	LING !
VARIANT	43	WID	TH REVISED	43	ліўтн	43	WIJTH	43	WIJTH
20/200		61	61	37	59	37	61	37	612
20/231	574	703	75%	51	682	51	753	53	フフシュ
70/248	545	72	762	47	70	49	762	49	フフシュ
70/260	512	73	フフキ	42	71	44	77之	45	792
60/236	582	732	78	51	712	53	78	54	792
170/273	49	74%	79	42	73	42	79	42	80
60/248	55	75	80	48	73	49	80	50	80
70/287	46	75%	802	382	74	382	8034	382	82
60/260	522	76	802	44	74	45	807	45	802
- 60/273	49%	772	812	42 1/2	752	422	81	43	81
50/236	59	772	82	55	75'	58	82:4	58	83
150/200	46	79	82	40	772	40	82	392	85
60/201	61	79	832	51	77	53	832	52'	84
20/248	100	0.4	45	47	78	49	85	49	87
50/260	53	802	86	42	80	- 44	2 86	44	872
50/273	47	83	87	40	81	1 42	87	412	882

INTERLOCK FABRICS

TABLE 5

SAMPLE	WB	WB	WD	WD
150/236	14.8	16.7	14.2	15. 1
150/248	15.8	13.4	15.5	15 0
150/260	16.3	16.7	16.6	15 -
150/273	18.8	13.8	17.9	15 1
150/287	19	13.9	17.9	16 1
160/236	17.7	14.2	15.4	15.4
160/248	20.3	12.4	16	13.4
160/260	18.8	13.4)17.2	14.9
160/273	19.3	15.1	17.5	16.
160/287	20.7	15	18.6	15.1
170/236	17.9	14.5	15.2	15.5
170/248	19.3	13.4	17.4	14.0.
170/260	20.8	13.6	19.6	12.7
170/273	23.4	1.2.1	20.1	14.9
170/287	23.9	11.1	19.7	15.3
138/338	19.2	16.6	19.7	15.8